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King Abdullah University of Science and Technology

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Identification of fracture properties for a cohesive model using digital image correlation

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Minneapolis, July 25th 2011

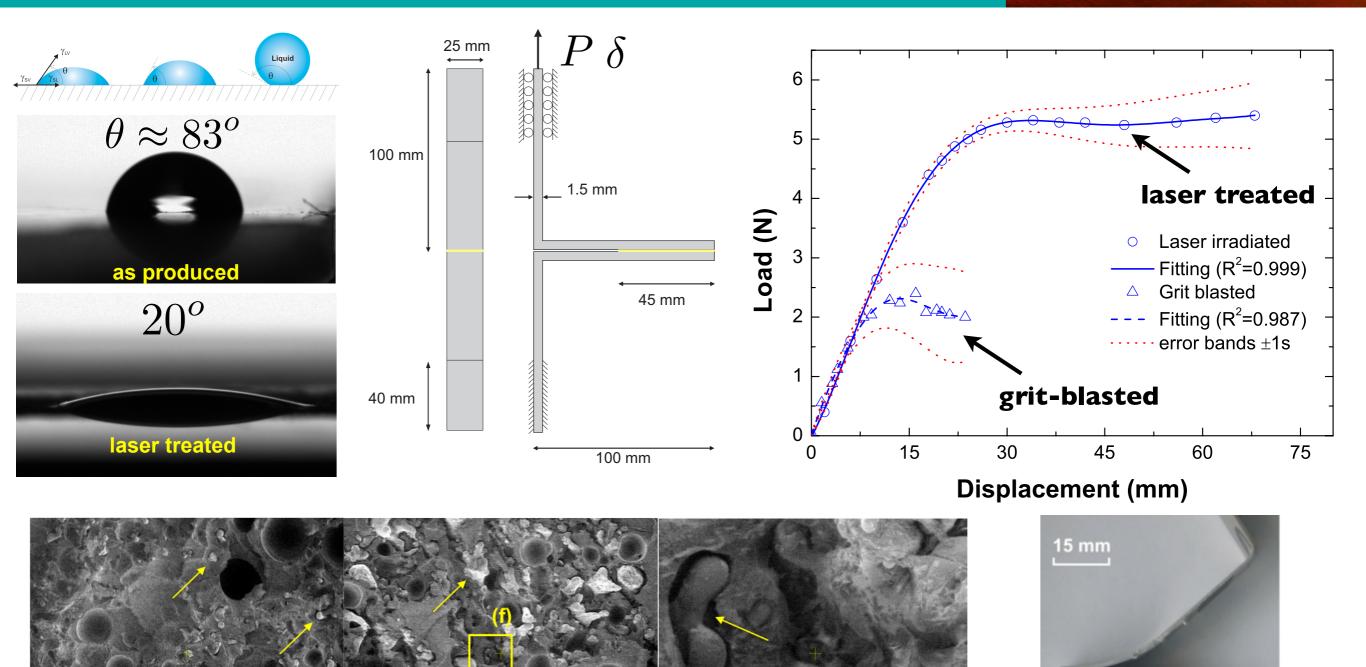
- 1. Introduction and motivation
- 2. Objective
- 3. Proposed approach
- 4. Algorithm and implementation of the inverse procedure
- 5. Target applications and experimental set-up (current status)
- 6. Follow-up work



Introduction and motivations (1/4)

Mechanical testing

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Alfano M, Furgiuele F, Lubineau G, Paulino GH. Role of laser surface preparation on damage and decohesion of Al/epoxy joints. *Submitted for Journal publication*.

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AI/AI-Laser-2

Introduction and motivations (2/4)

Units

N/m

MPa

μm

40

30

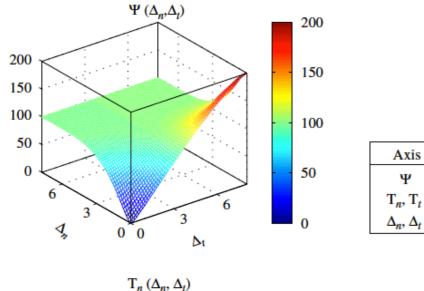
20

10

0

PPR based cohesive model

$$\Psi(\Delta_{n}, \Delta_{t}) = \min(\phi_{n}, \phi_{t}) + \left[\Gamma_{n}\left(1 - \frac{\Delta_{n}}{\delta_{n}}\right)^{\alpha}\left(\frac{m}{\alpha} + \frac{\Delta_{n}}{\delta_{n}}\right)^{m} + \langle\phi_{n} - \phi_{t}\rangle\right] \times \left[\Gamma_{t}\left(1 - \frac{|\Delta_{t}|}{\delta_{t}}\right)^{\beta}\left(\frac{n}{\beta} + \frac{|\Delta_{t}|}{\delta_{t}}\right)^{n} + \langle\phi_{t} - \phi_{n}\rangle\right].$$



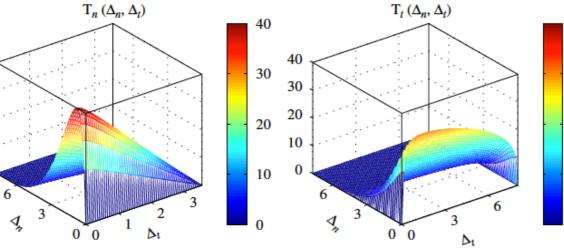
40

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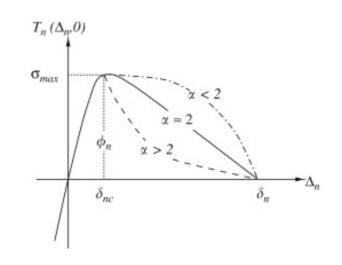
Park K, Paulino GH, Roesler JR. A unified potential-based cohesive model of mixed-mode fracture. *Journal of the Mechanics and Physics of Solids*. 2009;57(6):891-908.

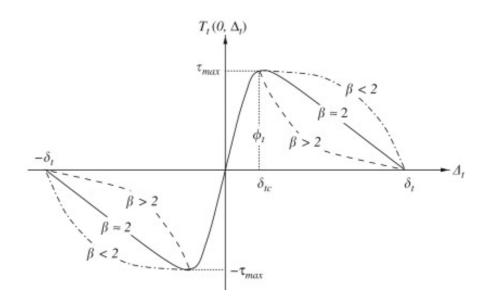
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- δ_n , δ_t characteristic length scale parameters
- $\bar{\delta}_n, \bar{\delta}_t$ normal and tangential conjugate final crack opening widths
- λ_{n}, λ_{t} initial slope indicators

 σ_{\max} , τ_{\max} normal and tangential cohesive strengths

- $\phi_{\rm n}, \phi_{\rm t}$ modes I and II fracture energies
- Ψ potential function for cohesive fracture
- α , β shape parameters in the PPR model





Introduction and motivations (3/4)

PPR for mode I fracture

$$\Psi(\Delta_n) = \phi_n + \Gamma_n \left(1 - \frac{\Delta_n}{\delta_n}\right)^{\alpha} \left(\frac{m}{\alpha} + \frac{\Delta_n}{\delta_n}\right)^m$$

$$\begin{aligned} T(\Delta_n) &= \frac{\partial \Psi}{\partial \Delta_n} = \\ &= \frac{\Gamma_n}{\delta_n} \left[m \left(1 - \frac{\Delta_n}{\delta_n} \right)^{\alpha} \left(\frac{m}{\alpha} + \frac{\Delta_n}{\delta_n} \right)^{m-1} - \alpha \left(1 - \frac{\Delta_n}{\delta_n} \right)^{\alpha-1} \left(\frac{m}{\alpha} + \frac{\Delta_n}{\delta_n} \right)^m \right] \end{aligned}$$

$$\Gamma_n = -\phi_n \left(\frac{\alpha}{m}\right)^m$$

$$m = \frac{\alpha \left(\alpha - 1\right) \lambda_n^2}{1 - \alpha \lambda_n^2}$$

$$\phi_n \to \omega \alpha^{-1} \left(\frac{\alpha}{m} - 1\right)$$

energy constant;

non-dimensional exponent;

 $\delta_n = \frac{\phi_n}{\sigma_{max}} \alpha \lambda_n \left(1 - \lambda_n\right)^{\alpha - 1} \left(\frac{\alpha}{m} + 1\right) \cdot \left(\frac{\alpha}{m} \lambda_n + 1\right)^{m - 1}$

final crack opening width;

$$\mathbf{X} = \{\phi_n, \sigma_{max}, \lambda_n, \alpha\}$$

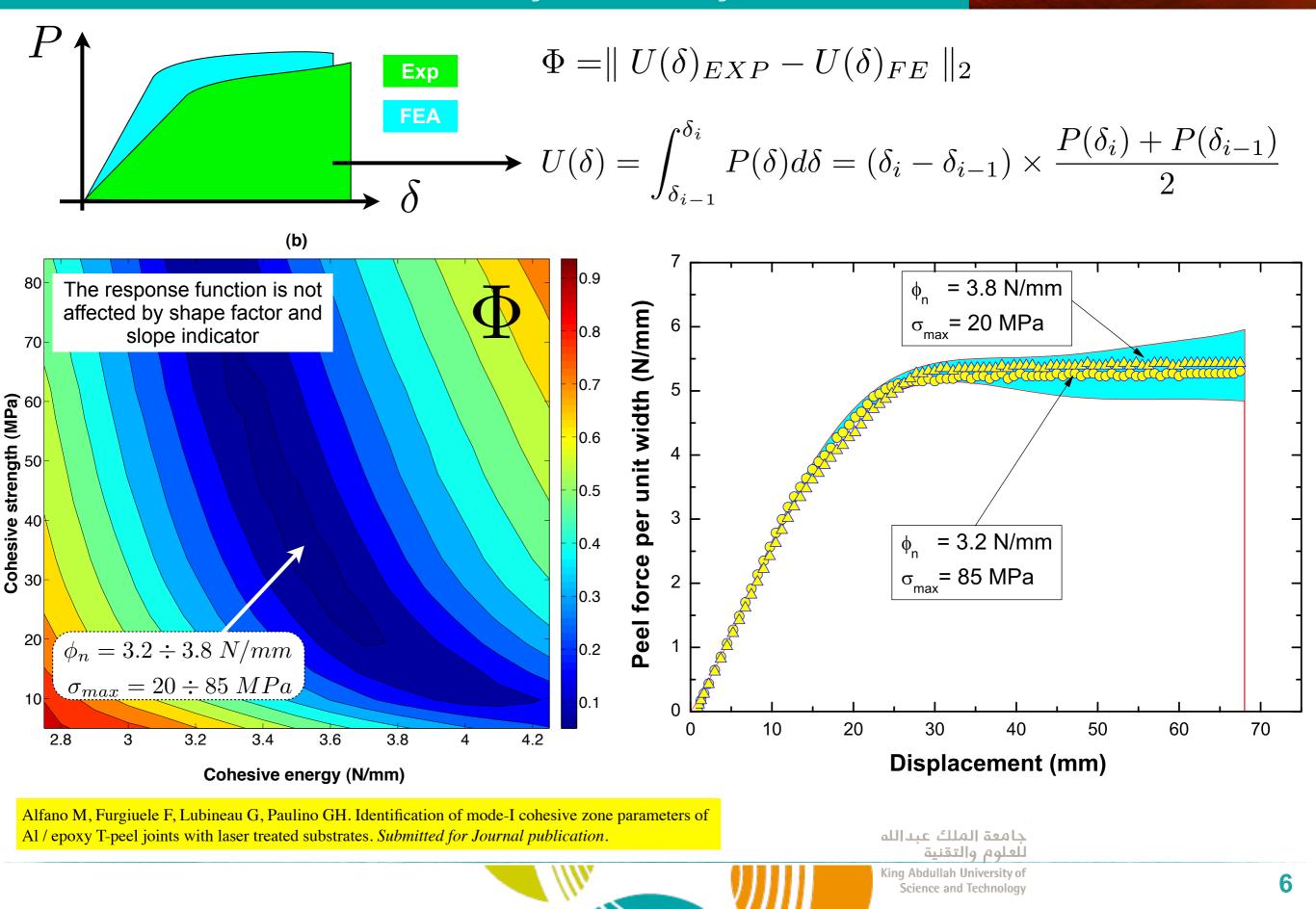
unknown properties to be identified

Park K, Paulino GH, Roesler JR. A unified potential-based cohesive model of mixed-mode fracture. *Journal of the Mechanics and Physics of Solids*. 2009;57(6):891-908.

Introduction and motivations (4/4)

Identification of bond toughness using the CZM

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➡ A global response is often obtained from experiments, however, it may have low sensitivity to certain cohesive properties.

➡The uniqueness of the obtained cohesive zone model is not guaranteed.

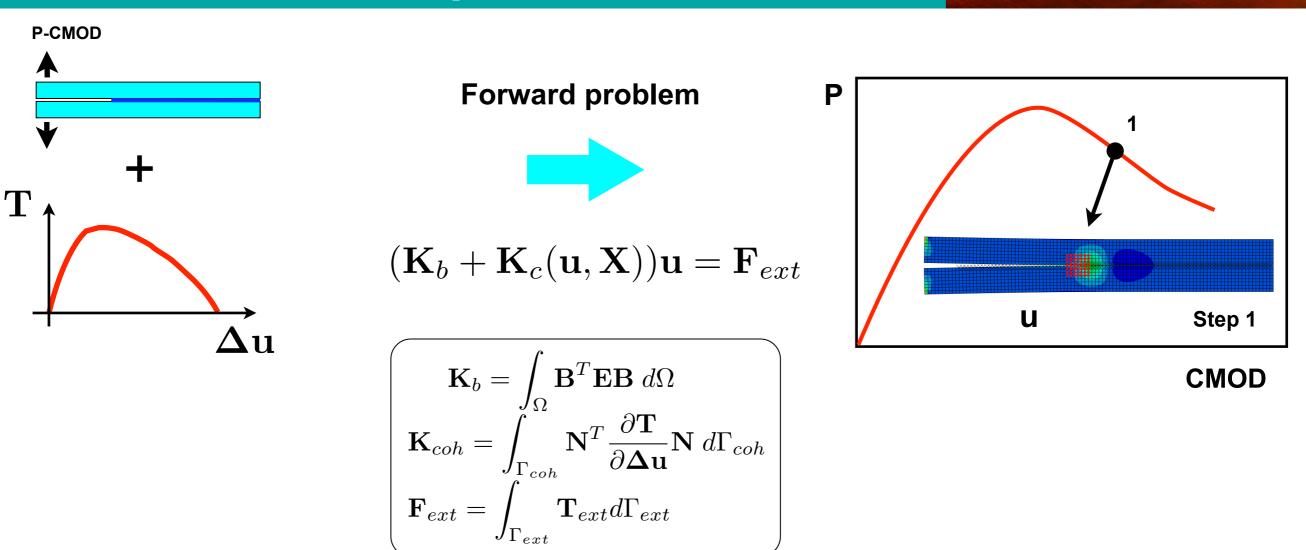
Although the cohesive models obtained using global data can yield satisfactory predictive capabilities in FEA simulations of fracture, the **development of an alternative procedure is needed**, e.g. to determine cohesive strength.

A solution may be provided by the original combination of experimental **full-field measurements** techniques and **inverse problems**.

Gain AL, Carroll J, Paulino GH, Lambros J. A hybrid experimental / numerical technique to extract cohesive fracture properties for mode-I fracture of quasi-brittle materials. *International Journal of Fracture*. 2011;169:113-131. Shen B, Paulino GH. Direct Extraction of Cohesive Fracture Properties from Digital Image Correlation: A Hybrid Inverse Technique. *Experimental Mechanics*. 2011;51(2):143-161.

Forward versus inverse problem

Forward problem



Principle of virtual work

$$\int_{\Omega} \boldsymbol{\sigma} : \delta \boldsymbol{\epsilon} \ d\Omega - \int_{\Gamma_{ext}} \mathbf{T}_{ext} \cdot \delta \boldsymbol{\Delta} \boldsymbol{u} \ d\Gamma_{ext} + \int_{\Gamma_{coh}} \mathbf{T}_{coh} \cdot \delta \boldsymbol{\Delta} \boldsymbol{u} \ d\Gamma_{coh} = 0$$

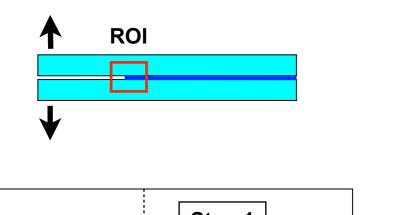
 $\begin{array}{l} \Omega: \text{specimen domain} \\ \Gamma_{ext}: \text{external boundary} \\ \Gamma_{coh}: \text{cohesive surfaces} \\ \boldsymbol{\Delta u}: \text{cohesive surfaces opening displacement} \\ \boldsymbol{\sigma}: \text{stress tensor} \\ \boldsymbol{\epsilon}: \text{strain tensor} \end{array}$

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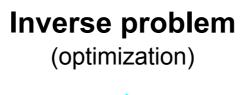
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Forward versus inverse problem

Inverse problem (objective of the work)



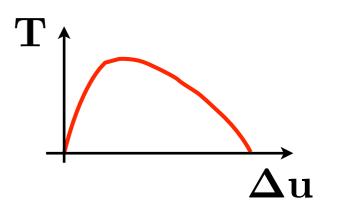
P-CMOD

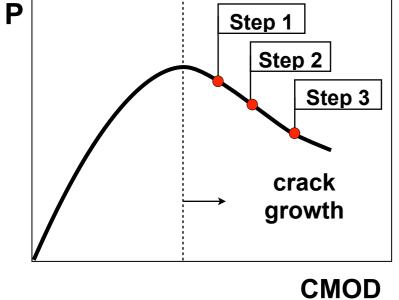




 $\hat{\mathbf{X}} = \underset{\mathbf{X} \in \mathbb{R}^{M}}{\arg\min} \{ \Pi = \sum_{i=1} \omega_{i} \left(\mathbf{X} \right) \}$

$$\mathbf{X} = \{\phi_n, \sigma_{max}, \alpha, \lambda_n\}$$





 $\omega_i (\mathbf{X}) = \frac{1}{(U_{max,i})^2} \sum_{j=1}^{n_n} [u_{exp} - u(\mathbf{X})]_j^2$ m: available measurement instants (load levels) n_n : nodal displacements in the ROI

$$egin{aligned} \mathbf{u}(\mathbf{X}) = \mathbf{K}_b^{-1} \hat{\mathbf{F}}^{ext}(\mathbf{u}_{exp} \ ; \mathbf{X}) \ \hat{\mathbf{F}}^{ext}(\mathbf{u}_{exp} \ ; \mathbf{X}) = \mathbf{F}^{ext} - \mathbf{K}_c(\mathbf{u}_{exp} \ ; \mathbf{X}) \mathbf{u}_{exp} \end{pmatrix}$$

Optimization algorithm?

Exploration algorithm based on the mechanism of natural selection and genetics: the strongest **individuals (chromosomes)** in a **population** survive and generate offsprings.

A **chromosome** represents a generic solution of the problem, in our context a set of cohesive fracture parameters (**X**):

X
$$\Phi_n$$
 σ_{max} λ_n α

Basic steps of the GA

1. Random generation of the **initial population** (individuals **X**) satisfying suitable restraint conditions (e.g. fracture energy must not be negative);

2. The chromosomes are evaluated, using some measures of **fitness**. We defined the following **objective function (or cost function)**:

$$\begin{split} \omega_{i}\left(\mathbf{X}\right) &= \frac{1}{\left(U_{max,i}\right)^{2}} \sum_{j=1}^{n_{n}} \left[u_{exp} - u\left(\mathbf{X}\right)\right]_{j}^{2} \\ \hat{\mathbf{X}} &= \operatorname*{arg\,min}_{\mathbf{X} \in \mathbb{R}^{M}} \{\Pi = \sum_{i=1}^{m} \omega_{i}\left(\mathbf{X}\right)\} \\ m : \text{ available measurement instants (load levels)} \\ n_{n} : \text{ nodal displacements in the ROI} \end{split}$$

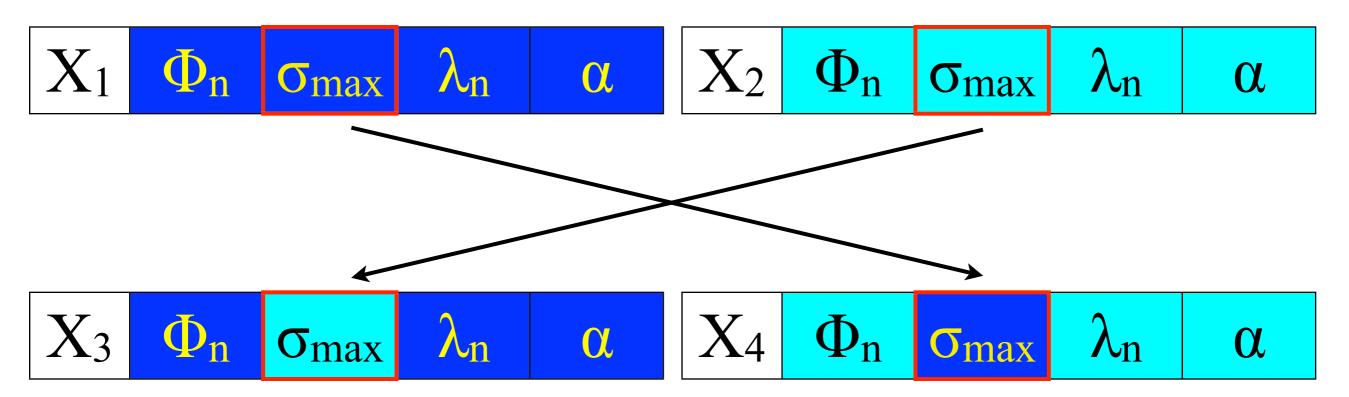
3. Individuals for **reproduction** are firstly chosen based on their fitness

4. and some of them are processed by means of **genetic operators** (crossover and mutation) to create a new populations

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5. New chromosomes, called **offspring**, are formed by merging two chromosomes from current generation

Crossover (type 1)

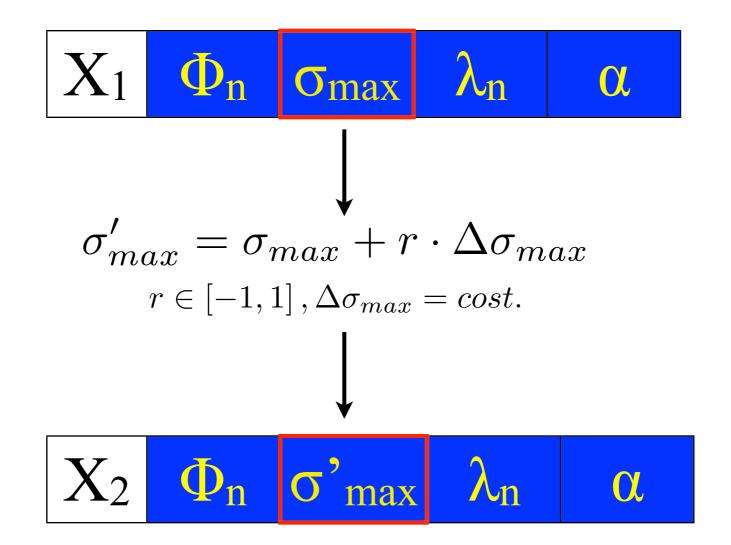


Crossover (type 2)

$$\mathbf{X}_3 = a \cdot \mathbf{X}_1 + (1 - a) \cdot \mathbf{X}_2$$
$$\mathbf{X}_4 = (1 - a) \cdot \mathbf{X}_1 + a \cdot \mathbf{X}_2$$

$$a \in [0,1]$$

5. New chromosomes are also formed by modifying a chromosome using a mutation operator

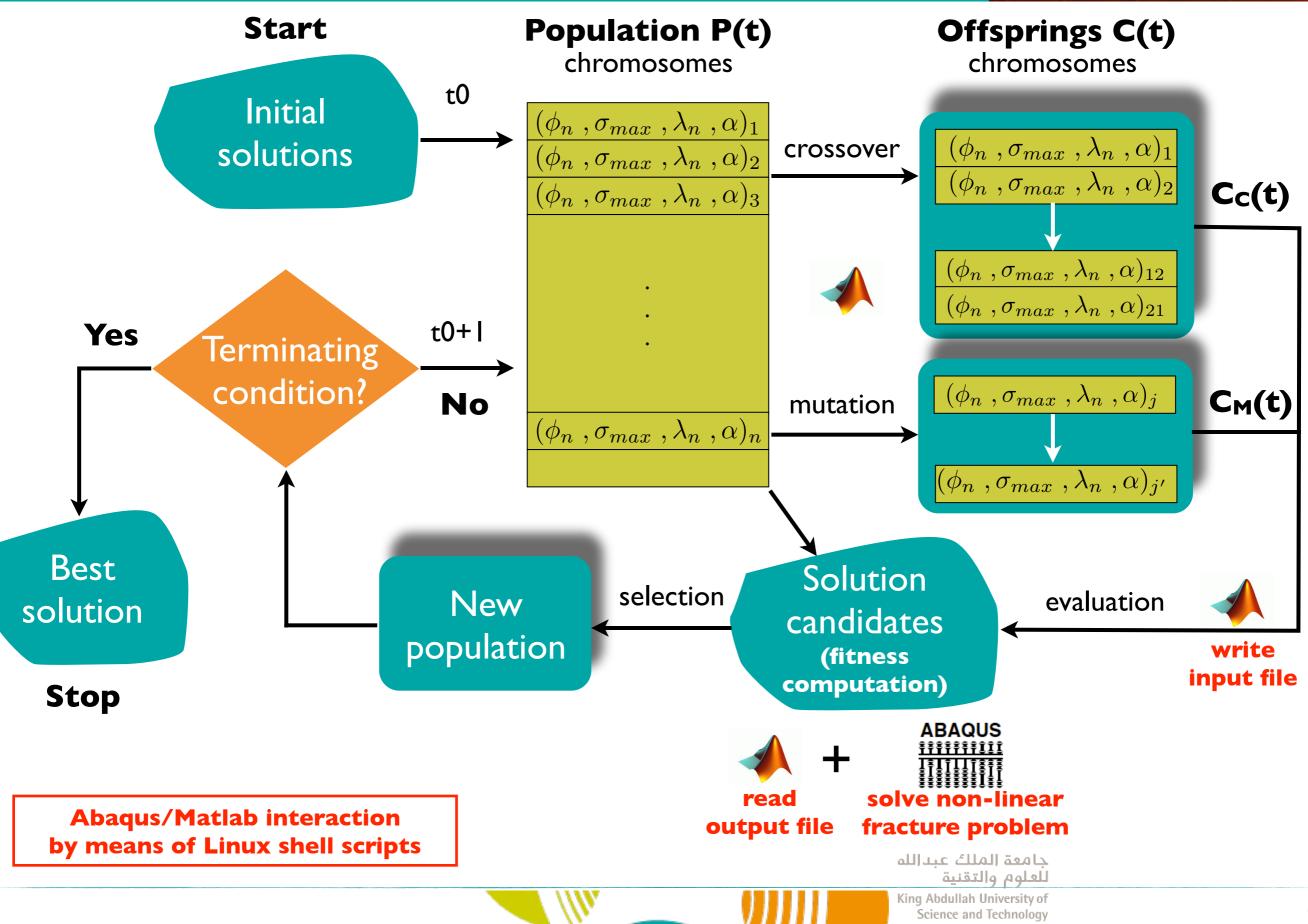


6. The newly created population replace the old one and the process restarts.

Genetic algorithm

Fundamentals concepts

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Target applications and experimental set-up

current status

Material processing - DCB with metal and composites substrates



Full-field experimental measurements



(http://cohmas.kaust.edu.sa)

Science and Technology



